

## **Note**

# **Specific Heat Capacity of Solids under Pressure from Measurements of $(\partial T/\partial P)_S$**

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A procedure is described for calculating specific heat capacity under pressure,  $c_p(T, P)$ , from data for  $c_p(T, 0)$  and adiabatic  $(\partial T/\partial P)_S$ . The main advantage is that  $(\partial T/\partial P)_S$  can be readily measured under high-pressure conditions.

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**KEY WORDS:** adiabatic compression; calculational procedure; high pressure; specific heat capacity.

## **1. INTRODUCTION**

Heat capacity under pressure is a difficult measurement, and there are so far relatively few results (see reviews by Bäckström [1] and Loriers-Susse [2]). On the other hand, there exist extensive results at effectively zero pressure for specific heat capacity at constant pressure as a function of temperature,  $c_p(T, 0)$  (see the compilation by Touloukian and Buyco [3]). The purpose of the present note is to describe how the relatively simple measurement of  $(\partial T/\partial P)_S$  under pressure enables data for  $c_p(T, 0)$  to be extended to high-pressure conditions.

## **2. DESCRIPTION OF THE PROCEDURE**

A method for measurement of the rate of change of temperature with pressure at constant entropy,  $(\partial T/\partial P)_S$ , has been described by Boehler et al.

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[4]. A solid specimen of the substance under investigation is arranged to have a thermocouple junction immersed in it at a central location. The specimen is then coated with an elastomer and placed in the pressure-transmitting medium in a pressure vessel. A sufficiently rapid change of pressure yields a  $T, P$  trajectory which is effectively adiabatic. The temperature is measured using the thermocouple located within the specimen and the pressure is measured using a manganin resistance gauge located in the pressure-transmitting medium.

Figure 1 shows a  $T, P$  projection which may be taken to refer to the central part of the specimen. It is assumed that  $c_p(T, 0)$  is known from  $T_{\min}$  to  $T_{\max}$  and that the lines in Fig. 1 labeled  $s_1, s_2, \dots, s_n$  correspond to the results of adiabatic experiments of the type just described. It can be assumed that the specific entropy  $s(T, 0)$  is also known, apart from a constant term, since

$$s(T, 0) = s(T_{\min}, 0) + \int_{T_{\min}}^T c_p(T', 0) d \ln T' \quad (1)$$

It follows that the entropies  $s_1, s_2, \dots, s_n$  of the adiabats are also known from the intercept of each adiabat with the axis  $P = 0$ . We now consider the

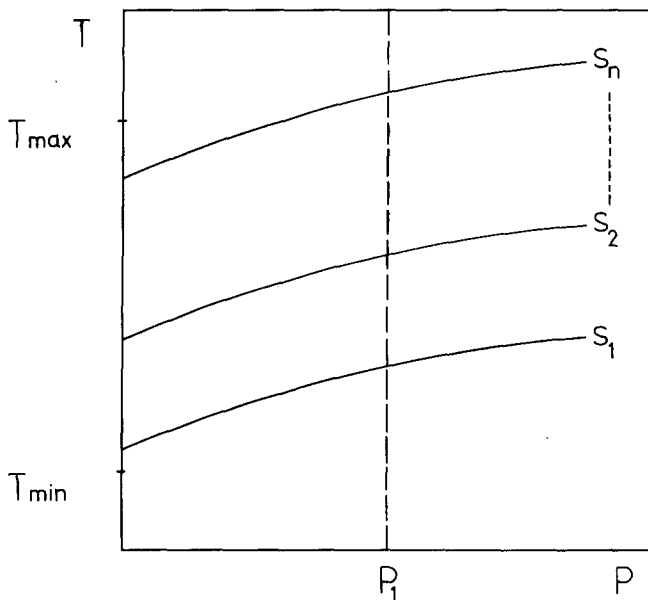


Fig. 1.  $T, P$  projection for substance under investigation.  $c_p(T, 0)$  is assumed to be known over the temperature range  $T_{\min}$  to  $T_{\max}$ . Lines labeled  $s_1, s_2, \dots, s_n$  are from measurements of  $(\partial T / \partial P)_s$ . Dashed line indicates isobar at  $P = P_1$ .

intersections of some isobar at  $P = P_1$  with the adiabats and, thereby, obtain a discrete set of data points which represents the function  $s(T, P_1)$ . Suitable differentiation then yields  $c_p(T, P_1)$  and the calculation can be repeated for a number of different isobars to yield a data set for  $c_p(T, P)$ .

While the discussion just given illustrates the principles, a practical calculation could proceed as follows. We have

$$\left(\frac{\partial T}{\partial P}\right)_s = \frac{\alpha T v}{c_p} = \frac{T}{c_p} \left(\frac{\partial v}{\partial T}\right)_p \quad (2)$$

where  $\alpha$  is thermal expansivity and  $v$  is specific volume. By setting  $T^{-1}(\partial T/\partial P)_s = f(T, P)$  and  $(\partial v/\partial T)_p = D(T, P)$ , we obtain

$$f c_p = D(T, P) \quad (3)$$

the function  $f$  being measurable. Now

$$c_p(T, P) = c_p(T, 0) + \int_0^P \left(\frac{\partial c_p}{\partial P'}\right)_T dP' = c_p(T, 0) - T \int_0^P \left(\frac{\partial^2 v}{\partial T^2}\right)_{p'} dP' \quad (4)$$

Hence

$$f c_p(T, 0) - f T \int_0^P \left(\frac{\partial D}{\partial T}\right)_{p'} dP' = D$$

or

$$F_0 - F_1 \int_0^P \left(\frac{\partial D}{\partial T}\right)_{p'} dP' = D \quad (5)$$

where

$$F_0 = f c_p(T, 0) = T^{-1} \left(\frac{\partial T}{\partial P}\right)_s c_p(T, 0)$$

and

$$F_1 = f T = \left(\frac{\partial T}{\partial P}\right)_s$$

$F_0$  and  $F_1$  are known experimentally at discrete values of  $T, P$  so the problem reduces to solving Eq. (5) for  $D(T, P)$ . The desired result,  $c_p(T, P)$ , then follows from Eq. (3).

The quantity  $D(T, P)$  may be represented by a polynomial in  $T$  and  $P$ . For purposes of illustration we neglect terms higher than quadratic and employ the relation

$$D(T, P) = D_{00} + D_{10}T + D_{01}P + D_{20}T^2 + D_{11}TP + D_{02}P^2 \quad (6)$$

Equation (5) then becomes

$$\begin{aligned} D_{00} + D_{10}(T + F_1P) + D_{01}P + D_{20}(T^2 + 2F_1TP) \\ + D_{11}(TP + F_1P^2/2) + D_{02}P^2 = F_0 \end{aligned} \quad (7)$$

The six coefficients  $D_{ij}$  may be obtained by taking experimental data for six points in the  $T, P$  plane. The resulting system of equations is linear in the coefficients  $D_{ij}$  and will remain so whatever the order of the polynomial assumed for  $D(T, P)$ . In a realistic case there will be many more data points than coefficients to determine. Therefore the best procedure would probably be to minimize

$$\sum_k \left[ F_0 - F_1 \int_0^P \left( \frac{\partial D}{\partial T} \right)_{P'} dP' - D \right]^2$$

with respect to the coefficients  $D_{ij}$ , the sum being taken over the experimental data points ( $k$ ).

### 3. DISCUSSION

The main advantage of the procedure described here is that the quantity required under pressure,  $(\partial T/\partial P)_S$ , is relatively easy to measure with good accuracy. In the experiments of Boehler et al. [4] it appears [5] that the inaccuracy in this quantity was  $\pm 1\%$  at pressures up to about 3 GPa at room temperature. Similar measurements have been described by Sandberg and Bäckström [6] and Dzhavadov and Krotov [7]. If  $c_p(T, 0)$  should not be known for some substance of interest, then it is readily measurable by, say, differential scanning calorimetry, a technique which can employ commercially available equipment.

Although we are concerned here mainly with  $c_p(T, P)$ , we point out that if  $v(T_0, P)$  along an isotherm ( $T_0$ ) is also known for the substance under investigation, then values for  $D(T, P)$  imply knowledge of the thermal expansivity  $\alpha = v^{-1}(\partial v/\partial T)_P$  and  $v(T, P)$  over the ranges of  $T$  and  $P$  for which measurements of  $(\partial T/\partial P)_S$  have been made.

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**REFERENCES**

1. G. Bäckström, in *Proc. Seven. Symp. Thermophys. Prob.*, A. Cezairliyan, ed. (American Society of Mechanical Engineers, New York, 1977), pp. 169–180.
2. C. Loriers-Susse, *High Temp. High Press.* **12**:119 (1980).
3. Y. S. Touloukian and E. H. Buyco, *Thermophysical Properties of Matter, Vol. 5. Specific Heat, Nonmetallic Solids* (IFI/Plenum, New York, 1970).
4. R. Boehler, I. C. Getting, and G. C. Kennedy, *J. Phys. Chem. Solids* **38**:233 (1977).
5. R. Boehler and J. Ramakrishnan, *J. Geophys. Res.* **85**:6996 (1980).
6. O. Sandberg and G. Bäckström, *J. Appl. Phys.* **50**:4720 (1979).
7. L. N. Dzhavadov and Yu. I. Krotov, *Sov. Phys. Solid State* **22**:172 (1980).